

The Self-assembly of Sepiolite and Silica Fillers

for Advanced Rubber Materials:

The Role of Collaborative Filler Network

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Abstract

Composite materials based on hybrid filler systems can be a promising approach to produce advanced rubber nanocomposites (NCs). Recently, the positive effect of the combined use of silica

23 and sepiolite on NCs mechanical properties has been reported, compared to those of compounds
24 reinforced with the same amount of the only silica filler. In this context, the present work aims at
25 studying the possible synergistic self-assembly of nanosilica and sepiolite in the generation of a
26 cooperative hybrid filler network in rubber-based NCs, in connection with material performance for
27 tires application. In detail, the influence of the introduction of a secondary anisotropic filler in
28 conjunction with isotropic nanosilica on their dispersion and interaction with the rubber matrix has
29 been comprehensively investigated, in order to define the best formulation ensuring low rolling
30 resistance and significant fuel saving.

31 NCs, containing simultaneously silica and sepiolite, either pristine (Sep) or chemically modified
32 (mSep) by an acid treatment, were prepared by combining latex compounding (LCT) and melt
33 blending techniques. Rheological and dynamic-mechanical analyses highlighted that the use of a
34 double white filler, constituted by particles with different aspect ratio, affords a good balance
35 between efficient reinforcement and low Payne effect.

36 TEM analysis evidenced the formation, within the rubber matrix, of cooperative superstructures due
37 to the self-assembly of sepiolite and silica nanoparticles containing occluded rubber, when the
38 secondary filler is mSep. The peculiar characteristics of mSep, characterized by fibers shorter than
39 Sep and higher surface silanol bonding sites, bring about significant interactions between mSep and
40 silica, which promote self-assembly of the two fillers in a collaborative hybrid network, improving
41 dynamic-mechanical performances.

42 These results, even if related to sepiolite/silica NCs, demonstrate the effective role of the
43 collaborative filler network, based on the hybrid double fillers, able to lend enhanced properties to
44 rubber materials.

45

46 **1. Introduction**

47 Composite materials based on hybrid filler systems (Galimberti et al., 2017a), i.e. the combination
48 of two or more type of fillers with different size and morphology, can be considered a promising
49 alternative to conventional nanocomposites (NCs). Hybrid fillers can indeed improve the dispersion
50 of each single filler in the polymer matrix which creates bridges among the particles, endowing an
51 easier formation a percolative network, with remarkable benefits on the composite rheological
52 properties (Galimberti et al., 2017a).

53 In the field of rubber-based NCs, the objective entailed in the use of hybrid fillers is to favor the
54 nanoparticles self-assembly in a collaborative filler network (Scotti et al., 2014; Tadiello et al.,
55 2015) involving the interactions of both fillers with the polymer matrix (Tripaldi et al., 2021),
56 providing either higher polymer–filler interactions and tailored filler–filler interactions (Redaelli et
57 al., 2018). It has been revealed that, besides the vulcanization process (Susanna et al., 2017;
58 Mostoni et al., 2019), the fillers compatibility and the cooperative interactions at the nanoscale level
59 lead to improved dynamic properties of rubber compounds, that is lower hysteresis at high
60 temperatures, that imparts to tyres lower rolling resistance and, in perspective, lead to lower fuel
61 consumption impacting on the transport costs (D’Arienzo et al., 2017).

62 For many years, the combination of silica and carbon black (CB) has been largely studied to exploit
63 the advantages of both fillers in the rubber compounds. At first, the use of mixed fillers focused on
64 the preparation of dual fillers based on a complex synthesis where silica particles are *in situ*
65 generated in a CB matrix (Wang and Zhao, 2010). Successively, different authors (Feng et al.,
66 2015; Senthilvel et al., 2016) demonstrated that the addition of small amounts of silica into CB
67 rubber compounds decreases the filler cluster branching and increases the reinforcement efficiency,
68 while higher silica loadings induce segregation phenomena, causing a deterioration in the filler–
69 rubber interface and consequently in the rubber properties.

70 Based on this experimental evidence, tire industry has developed the use of hybrid filler systems,
71 where CB is only partially substituted by precipitated silica functionalized with silane coupling

72 agents (Uhrlandt and Blume, 2001; Feng et al., 2015). These rubber compounds show improved
73 dynamic response at low and high temperatures with respect to those reinforced solely with CB,
74 which results in better rolling resistance and enhanced wet grip, while keeping satisfactory abrasion
75 resistance. Also clay fillers, have been extensively investigated in combination with CB (Das et al.,
76 2010; Galimberti et al., 2012), demonstrating that the anisotropic silica particles are critical to
77 create a hybrid filler network in the presence of a nano-structured filler, such as CB, and revealing a
78 significant affinity for the carbonaceous filler, prompting the enhancement of the filler networking
79 phenomenon.

80 The above reported literature foreshadows that the improvement of mechanical properties in hybrid
81 *filled composite materials* enclosing CB and silica is basically connected to the better dispersion of
82 both fillers in the polymer matrix, which avoids the filler flocculation phenomenon (Mora-Barrantes
83 et al., 2011). In the other words, the mixed reinforcing systems with CB reduce the entropic
84 contribution, since the presence of fillers with different surface characteristics reduces their natural
85 tendency to aggregate due to kinetic causes.

86 However, the behavior of rubber matrices reinforced with hybrid networks constituted exclusively
87 by white fillers, has been rarely investigated. Bokobza et al., 2009 reported the effect of mixing
88 organophilic sepiolite and silanized fumed silica on the mechanical behavior of styrene–butadiene
89 rubber. In this case, a toluene dispersion of both fillers were added to a toluene solution of rubber.
90 Final composites, containing 10 phr (parts per hundred rubber) of fillers, showed slightly enhanced
91 properties compared to those of compounds reinforced with the same amount of the only silica
92 filler. Nevertheless, the requirements of rubber matrix dissolution and low filler contents limits the
93 extension of this methodology toward large scale applications.

94 Silica and modified montmorillonite were investigated as double fillers into natural rubber (NR)
95 matrix, producing better stability of elastic modulus with temperature and an enhancement of
96 stresses at all elongations (Galimberti et al., 2017b). The authors suggested a synergistic effect
97 among fillers due to different aspect ratios (ARs) but, at last, they attributed the positive results to

98 the reduction of filler flocculation. Moreover, also in this case, the better performances are observed
99 in the presence of low amount of anisotropic filler.

100 Actually, it is well known that anisotropic fillers improve the dynamic-mechanical behavior of the
101 rubber NCs (Scotti et al., 2014; Tadiello et al., 2015) reducing the energy dissipation and, thus, the
102 fuel consumption. This effect has been mainly ascribed to the formation of the nanoscale rigid
103 rubber at the interface with the filler.

104 In view of these considerations, the clay/silica hybrid systems could be a possible strategy to further
105 reduce the hysteresis of rubber materials, due to the potential synergistic effect between isotropic
106 and anisotropic fillers in constituting a collaborative network. Actually, in the last decade, our
107 group has focused the research activity on the use of sepiolite filler in rubber NCs to improve the
108 mechanical properties of rubber materials (Giannini et al., 2016, 2018; Di Credico et al., 2018,
109 2019; Cobani et al., 2019; Tagliaro et al., 2020). In particular, we have recently reported on the
110 preparation of polymer NCs based on nano-sized sepiolite fibers (Cobani et al., 2019), obtained by
111 applying a controlled surface acid treatment on both pristine and organically-modified sepiolites.
112 These nanosized Sep fibers, having reduced particle size and improved density of the surface silanol
113 groups, provide, when embedded in rubber matrix, an excellent balance between reinforcing and
114 hysteretic behavior, compared to the large-sized pristine Sep and isotropic silica. This has been
115 attributed to the self-assembly of the anisotropic nanofibers in rigid filler network domains (Cobani,
116 2018; Cobani et al., 2019). Furthermore, nanosized sepiolite formulated with silica and CB in
117 technical compositions for vulcanisable elastomeric materials produced a remarkable decrease of
118 Payne effect and hysteresis while maintaining a good reinforcement of the elastomeric materials
119 (Giannini et al., 2016; Di Credico et al., 2018; Tadiello et al., 2018).

120 Although several studies clearly showed that dual filler systems composed by silica and sepiolite
121 positively impact on the properties of rubber composite (Bokobza, 2006; Locatelli et al., 2020;
122 Staropoli et al., 2021), also in the presence of CB (Mohanty et al., 2021), to the best of our
123 knowledge no work has yet systematically investigated the direct relationship between the synergic

124 interaction of different fillers in the network and the final material properties. Thus, there is a lack
125 of studies which clearly demonstrate the occurrence of an effective cooperative filler network, with
126 an interconnected structure of both clays and silica particles which experience direct interactions as
127 well as their bridging by rubber chains.

128 In this context, the present work aims at exploring the possibility of a synergistic interaction
129 between silica nanoparticles and different kinds of sepiolite fillers in the generation of a
130 collaborative SiO₂/sepiolite hybrid network. In particular, the influence of the introduction of a
131 secondary anisotropic filler in combination with isotropic silica on the filler dispersion and filler-
132 rubber interactions will be further investigated, in order to attain a better tire performance in terms
133 of lower rolling resistance and fuel saving.

134 Sepiolite fibers, previously modified with *N*-C14-18-alkyl-*N,N*-dimethylbenzylammonium (Sep),
135 were selected to study the role of the organically modified Sep in promoting hybrid filler
136 networking with silica. While the choice of this clay is tied to its good reinforcing properties, due to
137 the high AR, the organic modifier is essential to enhance interfacial rubber/filler adhesion,
138 considering the low compatibility between rubber and sepiolite, as already demonstrated in our
139 previous study (Di Credico et al., 2018). On the other hand, although the organically-modified clays
140 show better dispersion in a polymer matrix, the polymer-filler interaction is generally not improved
141 because of the presence of hydrophilic silanol groups on the Sep surface. Along this line, the above
142 mentioned Sep filler chemically modified by a controlled acid modification (mSep) was also
143 investigated, since it presents an increased amount of surface silanols and decreased fiber size,
144 which both favor the interfacial interactions with the polymer and the formation of filler network
145 structure (Di Credico et al., 2018).

146 Rubber-based NCs containing silica and sepiolite were prepared by combining latex compounding
147 technique (LCT) and melt blending. Highly filled NR masterbatches (MBs) were firstly prepared by
148 coagulating NR latex and sepiolite aqueous suspension, as previously reported (Di Credico et al.,
149 2019; Tagliaro et al., 2020). MBs were subsequently mixed with NR rubber matrix together with

150 silica filler, silane coupling agent, vulcanizing agents and antioxidants. This combined procedure is
151 convenient because it: i) improves the hydrophilic filler dispersion in the first stage, and ii) prevents
152 dust formation and filler loss during melt blending stage since the sepiolite fibers are previously
153 dispersed in NR MBs. Morphology, rheology and dynamic-mechanical properties of the achieved
154 NCs were compared with those of samples containing SiO₂, Sep, or mSep prepared by a traditional
155 melt blending procedure, in order to highlight the self-assembly effect of *hybrid filler systems* on
156 the final properties of the resulting materials. Moreover, the influence of the different fillers and of
157 the preparation techniques on the molecular mobility of NR in the NCs was investigated by ¹H
158 Time Domain Nuclear Magnetic Resonance (NMR).

159

160 **2. Experimental**

161 *2.1 Materials*

162 Sepiolite Pangel B5 (organically-modified with *N*-C14-18-alkyl-*N,N*-dimethylbenzylammonium,
163 Sep) was supplied by Tolsa and extracted from the landfill of Vallecas (Spain), while Silica Zeosil
164 MP1165 (BET specific surface area 160 m²g⁻¹ and average single particle dimension 22 nm) from
165 Solvay.

166 *Compounding of MBs and NCs:* NRL Medium Ammonia (MA) (60% w/w) was supplied by Von
167 Bundit. HCl (37% w/w) and NH₄OH (28-30% w/w) and isopropanol were purchased from Sigma-
168 Aldrich and used without any further purification.

169 NR is STR20 from Von Bundit; bis(3-triethoxysilylpropyl) tetrasulfide (TESPT) purchased from
170 Sigma-Aldrich; antioxidant *N*-(1,3-dimethylbutyl)-*N*-phenyl-*p*-phenyldiamine (6PPD), Santoflex-
171 6PPD; the curing agents were purchased as follows: Stearic acid (Stearina TP8) from Undesa;
172 sulfur from Zolfoindustria; zinc oxide (wurtzite, specific surface area 5 m² g⁻¹) from Zincol Ossidi;
173 *N*-cyclohexyl-2-benzothiazole sulfenamide (CBS) Vulkacit CZ/C from Lanxess. Milli-Q water with
174 a resistivity 18.2 MΩ cm was utilized.

175

176 *2.2 Preparation of mSep by acid treatment*

177 mSep was prepared according to a previously reported procedure (Giannini et al., 2018). 100 g of
178 pristine Sep were dispersed in 1.5 L of deionized water and stirred at 70 °C (600 revolution per
179 minute (rpm)). With an automatic pH-meter, 31 ml of aqueous 37% HCl were added over a period
180 of 7 hours, at 70 °C, maintaining the pH around 3.0 ± 0.1 . The resulting fibers were collected by
181 centrifugation and the powders were washed several times with deionized water and aqueous
182 ammonium hydroxide (60%) in order to remove chloride anions, until pH 7 ± 0.2 . Finally, the
183 obtained solid was dried in an oven at 100 °C for 48 h. From the X-ray fluorescence (XRF) analysis
184 of mSep samples, 35% by weight of magnesium resulted extracted (data previously reported in
185 Tadiello et al., 2018).

186

187 *2.3. Preparation of MBs*

188 Sep MB samples containing high amounts of filler were prepared according to a previously reported
189 procedure (Di Credico et al., 2019).

190 10 g of Sep (Sep or mSep) was dispersed in water (500 mL), sonicated for 30 min and then mixed
191 with a mechanical stirrer (Velp Scientifica Stirrer DLS) at 500 rpm. In another vessel, 16.7 g of
192 NRL-MA (corresponding to 10 g of dried NR) were diluted with 125 ml of distilled water and
193 stirred for 10 min at 100 rpm. Then, the diluted NRL solution was slowly poured into the previous
194 Sep dispersion, under stirring at 500 rpm until the flocculation of the Sep MBs (MB-Sep or MB-
195 mSep) was completed (30 s). Sep MBs were separated from the liquid phase through filtration,
196 washed with water to remove ammonium residuals, and portioned in small pieces. MB samples
197 were dried under nitrogen at 10-2 bar at 80 °C for 48 h.

198

199 *2.4 Preparation of NCs*

200 The composite materials were prepared incorporating MBs to NR matrix and other compounding
201 ingredients in a Brabender Plasti-Corder lab station internal mixer (65 mL mixing chamber, 0.6
202 filling factor) through thermomechanical blending.

203 The production of NC materials consists of three mixing steps. Times and temperatures were
204 selected according to the thermal stability of the reactants and to the workability of rubber. The
205 amount of filler (SiO_2 or SiO_2/Sep) was kept constant at 32 phr. In the first step, NR was masticated
206 at 120 °C and 60 rpm rotor speed for 30 s. Then, filler or MB were added together with TESPT (2.5
207 phr) to the masticated rubber in three subsequent aliquots and mixed. After two minutes of mixing,
208 6PPD (2 phr), zinc oxide (3.5 phr) and stearic acid (2 phr) were then added and masticated for
209 further 5 min. In the second step, the obtained compounds were reloaded in the mixing chamber and
210 masticated at 90 °C and 60 rpm for 3 min; sulfur (1 phr) and CBS (3 phr) were then added and
211 mixed for further 2 min. In the third step, the resultant materials were processed in a two-rolling
212 mill at 50 °C for 3 min for improving their homogeneity. Reference materials containing Silica
213 Zeosil 1165 (Solvay), Sep and mSep were prepared by this procedure.

214 Vulcanization process was performed in a hydraulic press at 170 °C and 100 bar for 10 min.

215 Cured composite materials, compounded starting from Sep and mSep are named Sep+ SiO_2/NR and
216 mSep+ SiO_2/NR , respectively; analogously, those compounded starting from MBs are called MB-
217 Sep+ SiO_2/NR and MB-mSep+ SiO_2/NR , respectively. Cured reference material, containing only
218 silica filler is labelled as SiO_2/NR . The compositions of the NCs are summarized in Table 1.

219

220 *2.5 Morphological characterization of cured NCs*

221 50 nm thick sections of all vulcanized composite materials were cut by a Leica EM FCS cryo-
222 ultramicrotome, equipped with a diamond knife, by keeping the samples frozen at -130 °C. The
223 morphology of vulcanized compounds was investigated at different magnifications by TEM
224 analysis with a Zeiss EM 900 microscope (80 kV).

225

226 **Table 1** Filler formulations of composite materials*

Sample	SiO ₂	Sep	mSep	TESPT	Stearic acid	6PPD	ZnO	CBS	S
SiO ₂ /NR	32	-	-	2.5	2	2	3.5	3	1
Sep+SiO ₂ /NR	16	16	-	2.5	2	2	3.5	3	1
MB-Sep+SiO ₂ /NR	16	16	-	2.5	2	2	3.5	3	1
mSep+SiO ₂ /NR	16	-	16	2.5	2	2	3.5	3	1
MB-mSep+SiO ₂ /NR	16	-	16	2.5	2	2	3.5	3	1

227 * Amount of ingredients expressed in phr (parts per hundred rubber)

228

229 *2.6 Dynamic-mechanical analysis composites*

230 Uncured materials were cut by using a Constant Volume Rubber Sample Cutter (CUTTER 2000,
231 Alpha Technologies) obtaining samples of 3.5 cm diameter, ≈ 0.2 cm thickness and 6 ± 0.3 g.

232 Curing was performed with a Rubber Process Analyzer (RPA2000, Alpha Technologies) under the
233 following conditions: oscillation angle $\pm 1^\circ$, 170 °C, 15.65 kPa for 10 min (time sufficient to reach
234 the curing plateau). The following parameters were obtained: M_L is the minimum torque measured,
235 M_H is the maximum torque measured, and the scorch time is the time needed to start the
236 vulcanization process.

237 After curing, vulcanized samples were analyzed by dynamic-mechanical measurements with the
238 same instrument applying a shear stress mode. Strain sweep experiments (0-10% strain) were
239 carried out at 70°C and 10 Hz. Five measurements were performed for each sample, and the
240 average value was reported.

241 The storage modulus (G') at different strain values was evaluated and discussed. To better
242 understand the variation in mechanical properties due to double hybrid fillers with respect to

243 standard nanosilica, we report the values of G' at 0,5% as G'_0 and G' at 10% as G'_∞ in order to
244 evaluate the reinforcement, Payne effect and hysteresis of rubber materials.

245

246 2.7 ^1H Time Domain NMR

247 ^1H Time Domain NMR measurements were performed at a Larmor frequency of 20.8 MHz using a
248 Niumag permanent magnet interfaced with a Stellar PC-NMR console. A 5 mm probe was used with
249 a ^1H 90° pulse duration of $\tau_{90} = 3 \mu\text{s}$ for all samples. On-resonance Free Induction Decays (FIDs)
250 were recorded for all samples and standard samples using the Magic Sandwich Echo (MSE) pulse
251 sequence (Rhim et al., 1971; Matsui, 1991) with a total echo duration of $\tau_{\text{MSE}} = 6(4\tau_\phi + 2\tau_{90}) = 72$
252 μs , with $\tau_\phi = 1.5 \mu\text{s}$, using a dwell time of $0.1 \mu\text{s}$ and 8k acquisition points; 300-800 scans were
253 accumulated using a recycle delay of 5 times the measured ^1H T_1 (3-10 s), in order to guarantee
254 quantitative measurements. For all composite materials and for pure compounds displaying a slowly
255 decaying component of the FID (NR and SiO_2), Carr-Purcell-Meiboom-Gill (CPMG) sequence
256 (Meiboom and Gill, 1958) was also acquired; 400 transients were accumulated acquiring 2000 data
257 points. For the construction of MSE/CPMG relaxation curves, the first 180 data points of the MSE
258 ^1H FID (recorded within the first 180 μs of the acquisition) were joined together with all the data
259 points of the CPMG experiment recorded after 180 μs of acquisition. In order to eliminate residual
260 water which could alter the results of the ^1H FID analysis of isolated components, Sep and SiO_2
261 samples were dried in an oven at 105°C for 16 hours before acquisition.

262 The experimental MSE ^1H FID's or the combined MSE/CPMG relaxation curves were analyzed by
263 a discrete approach using a non-linear least square fitting procedure implemented in the
264 Mathematica® environment (Wolfram Research Europe Ltd, Oxfordshire, United Kingdom).

265

266 3. Results and Discussion

267 Combined latex and melt blending compounding techniques were applied for preparing *hybrid*
268 *filled composite materials* containing both silica and sepiolite (Table 1).

269 Highly loaded MBs containing Sep or mSep were firstly prepared by co-coagulation of NR latex
270 and filler dispersions by LCT approach, in order to take advantage of good dispersion of both Sep
271 and mSep fillers in aqueous medium. In fact, since the Sep dispersion shows a positive zeta
272 potential, ascribable to the presence of the alkylammonium salt (Di Credico et al., 2019), this gives
273 rise to the fillers repulsion especially at high Sep concentration, favoring an efficient and stable
274 colloidal dispersion. This occurs also for mSep, where the ammonium salt is only partially removed
275 during acid treatment. In addition, mSep benefits also the enhanced hydrophilic silanol groups onto
276 filler surface.

277 In the subsequent step, MBs were compounded by melt blending with the NR rubber matrix and
278 silica filler together with silane, coupling agent, vulcanizing agents, and antioxidants.

279 The combined latex/melt blending approach is a valuable procedure for several reasons:

280 i) hydrophilic filler dispersion is improved; ii) filler loss during processing is reduced in case of
281 compounding filler with low bulk density, like Sep; iii) abrasion and scratching on blending
282 machines are inhibited, because the fillers are previously dispersed in NR MBs; iv) high processing
283 temperatures are avoided, since severe friction phenomena among filler particles are hindered.

284 A critical evaluation of the effect of hybrid filler systems on rheological and mechanical properties
285 of final NC materials was performed, considering as a reference a compound with silica as single
286 filler. In addition, the features of hybrid filler compounds obtained by the combined techniques
287 (MB-Sep+SiO₂/NR, MB-mSep+SiO₂/NR) were compared to those of NCs prepared by traditional
288 compounding (Sep+SiO₂/NR, mSep+SiO₂/NR), where both fillers were introduced by melt
289 blending.

290 The rheometric characteristics of hybrid filled NCs, expressed in terms of the minimum torque (M_L)
291 and the maximum torque (M_H), are reported in Table 2.

292 The scorch time, defined as the time needed for the vulcanization to start, is a crucial parameter for
293 the industrial moulding of the material (Susanna et al., 2017). As reported in Table 2, the scorch
294 time of all the samples varies in the range of 2.0 – 2.5 min. In particular, the scorch times of silica-

295 filled NR compounds with organoclay as co-fillers are slightly lower compared to the reference
 296 compound with silica alone. It is well known that free silanol groups on the silica surface interfere
 297 with the vulcanization process due to their acidic nature and their tendency to adsorb accelerators,
 298 thus retarding the vulcanization. In the case of the hybrid filler systems, the use of organoclays
 299 having a quaternary ammonium modifying agent protects the silanols groups decreasing the scorch
 300 time as reported by other authors (Sattayanurak et al., 2019). However, both Sep+SiO₂/NR and
 301 mSep+SiO₂/NR, the scorch time only slightly decreased and thus in line with the standard time
 302 required in the rubber industry.

303

304 **Table 2** Curing characteristic of rubber NCs.

	Scorch time (min)	M _L (dNm)	M _H (dNm)	M _H -M _L (dNm)
SiO₂/NR	2.5 (±0.2)	2.3 (±0.1)	15.8 (±0.2)	13.5 (±0.3)
Sep+SiO₂/NR	2.0 (±0.2)	2.0 (±0.1)	13.5 (±0.2)	11.5 (±0.3)
MB-Sep+SiO₂/NR	2.0 (±0.2)	2.1 (±0.2)	12.3 (±0.2)	10.2 (±0.4)
mSep+SiO₂/NR	2.3 (±0.2)	2.1 (±0.1)	12.9 (±0.3)	10.8 (±0.4)
MB-mSep+SiO₂/NR	2.0 (±0.2)	1.7 (±0.2)	11.6 (±0.2)	9.9 (±0.4)

305

306 Moreover, considering the high adsorption properties of these clay minerals, the comparable scorch
 307 times observed in all the samples is a proof of similar vulcanizing agent adsorption on both sepiolite
 308 and standard silica.

309 The minimum torque (M_L), which is the torque at the initial stage of the vulcanization process, can
 310 be considered a parameter related to viscosity. Generally, the samples containing sepiolite show
 311 slightly lower M_L compared to those containing silica alone. This could be related to free
 312 ammonium salt, contained in both nanofillers, which can act as lubricant and secondary accelerator
 313 of vulcanization (Di Credico et al., 2018).

314 At the same time, the lowest value of M_L of MB-mSep+SiO₂/NR could be attributed to the better
315 dispersion of filler mSep, having high amount of silanols after acid modification, by using LCT,
316 providing lower viscosity in the final NC.

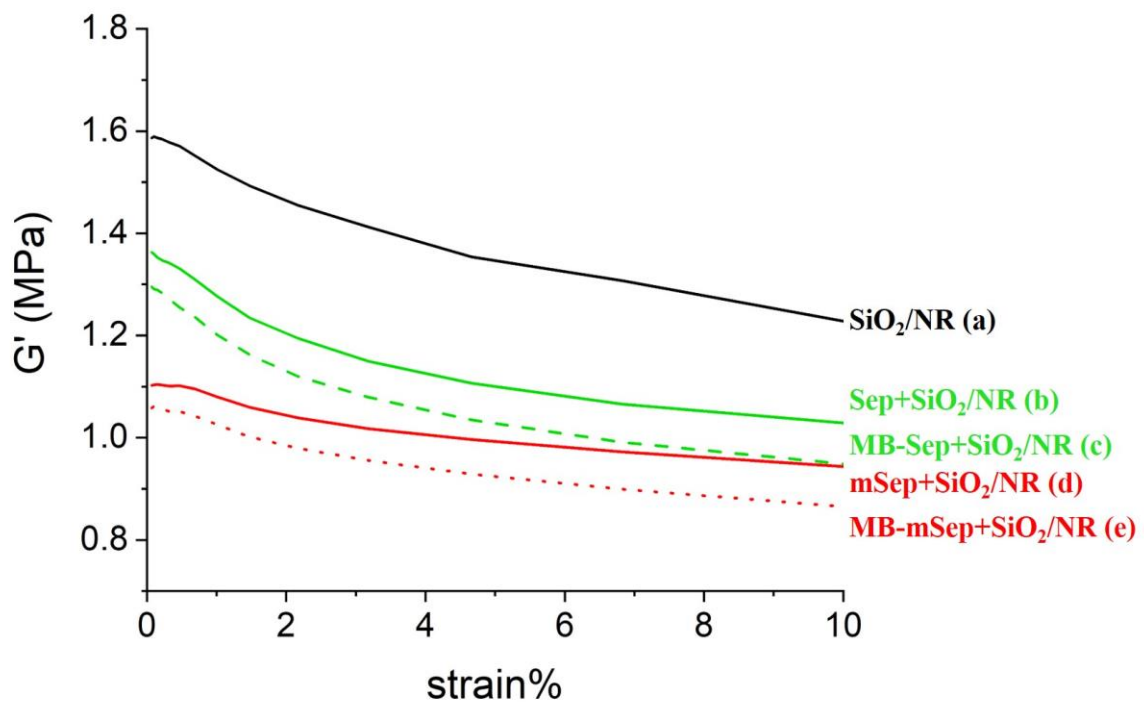
317 The presence of hybrid filler systems in NR matrix gives satisfactory values of the maximum torque
318 (M_H), which is a measure of the crosslink density and stiffness of the rubber, including also the
319 contribution of filler-network. In detail, the organoclay-containing compounds show a small
320 decrease in M_H and torque increment (which is the M_H-M_L), which may be again related to the
321 effect of the modifying agent of the organoclay and the desired decrease in filler networking. On the
322 other hand, it is noteworthy that the decrease of M_H value is almost irrelevant, especially in
323 comparison to the results recently reported by other authors (Sattayanurak et al., 2019), where a
324 considerable decrease in torque is observed even with the addition of small amounts of secondary
325 organoclay filler. Also, M_H value of the samples formulated by MB is not significantly influenced
326 by the combined compounding technique, proving the maintenance of the material properties. This
327 suggests that the material formulated by LCT was not corrupted by possible oxidation processes,
328 found in other cases during aqueous flocculation process in the presence of sepiolite (Carignani et
329 al., 2020). The high M_H-M_L value found for the SiO₂/NR sample confirms the excellent interaction
330 with the sulfur-based vulcanization compounds. With respect to this sample, the NCs containing
331 sepiolite show values slightly lower of about 2 dNm.

332 The impact of secondary filler on the mechanical properties of hybrid filled composites was studied
333 also by monitoring the dependence of the storage modulus (G') on the strain. The curves in Fig. 1
334 show: i) higher modulus at low strain (G'_0) value of SiO₂/NR (black line); ii) higher G'_0 and
335 modulus at high strain (G'_∞) values for the composites obtained by traditional melt blending with
336 respect to those obtained by MB; iii) $\Delta(G'_\infty-G'_0)$ values much lower in the samples containing both
337 mSep and SiO₂, independently on the preparation method (red and red dotted lines).

338 Table 3 reports dynamic parameters, *i.e.* the storage modulus G'_0 , the Payne effect $\Delta(G'_0-G'_\infty)$ and
339 loss factor as TanDelta (9%). G'_0 represents the filler-filler interaction and thus the measure of filler

340 reinforcement, while the so-called Payne effect is caused by the hysteretic breakdown at small
341 strains of the filler network derived by fillers joined together or through polymer layers. During
342 deformation, the hysteretic breakdown and reformation of the network is associated with the energy
343 dissipative process. In tires, this energy loss is the major contribution to the rolling resistance and
344 represents an undesirable effect, determining a high fuel consumption.(Cobani et al., 2019) In this
345 regard, TanDelta (9%) can be considered a good parameter for hysteresis estimation in vulcanized
346 rubber and thus an indication of the rolling resistance contribution of the compound (D'Arienzo et
347 al., 2018; Scotti et al., 2018).

348



349 **Fig. 1** Loss modulus G' vs strain of SiO₂/NR (a, black line), Sep+SiO₂/NR (b, green line), MB-
350 Sep+SiO₂/NR (c, green dashed line), mSep+SiO₂/NR (d, red line), MB-mSep+SiO₂/NR (e, red
351 dotted line).

352

353

354 **Table 3** Dynamic properties: storage modulus at low strain G'_0 , Payne effect as $\Delta(G'_0-G'_\infty)$, loss
355 factor as TanDelta (9%) of cured samples. Lettering refers to Fig.1.

	G'_0 (MPa)	$\Delta(G'_0-G'_\infty)$ (MPa)	TanDelta (9%)*
SiO₂/NR (a)	1.25 (\pm 0.05)	0.34 (\pm 0.02)	0.07 (\pm 0.01)
Sep+SiO₂/NR (b)	1.04 (\pm 0.05)	0.30 (\pm 0.02)	0.06 (\pm 0.01)
MB-Sep+SiO₂/NR (c)	0.96 (\pm 0.05)	0.30 (\pm 0.02)	0.07 (\pm 0.01)
mSep+SiO₂/NR (d)	0.95 (\pm 0.05)	0.16 (\pm 0.02)	0.05 (\pm 0.01)
MB-mSep+SiO₂/NR (e)	0.88 (\pm 0.05)	0.19 (\pm 0.02)	0.07 (\pm 0.01)

356

357 *Calculated as ratio of the G' and storage modulus (G'') at 9 % of strain.

358

359 SiO₂/NR sample shows the highest G'_0 value, suggesting a remarkable interaction among filler
360 particles. The presence of double fillers produces only a slight decrease in the reinforcement, which
361 remains in the same range of that of SiO₂/NR composite.

362 Interestingly, the Payne effect of NCs containing both silica and sepiolite is reduced with respect to
363 that containing only commercial silica (SiO₂/NR sample). In particular, samples with mSep, *i.e.*
364 mSep+SiO₂/NR and MB-mSep+SiO₂/NR, display significantly low Payne effect values.

365 In addition, the dynamic loss tangent in mSep+SiO₂/NR is reduced (0.05) compared to composites
366 including both silica alone (0.07) and untreated Sep (0.06), suggesting that double fillers promote
367 the filler-rubber interactions, particularly when Sep is modified by acid treatment (mSep). This is
368 supported also by lower values of the loss modulus (Fig. S1) for mSep+SiO₂/NR and MB-
369 mSep+SiO₂/NR, at small and high strains, indicating a significant reduction of the energy
370 dissipation during deformation, and the improvement of breakage and rebuilding of filler-filler
371 network and slippage of the polymer chains.

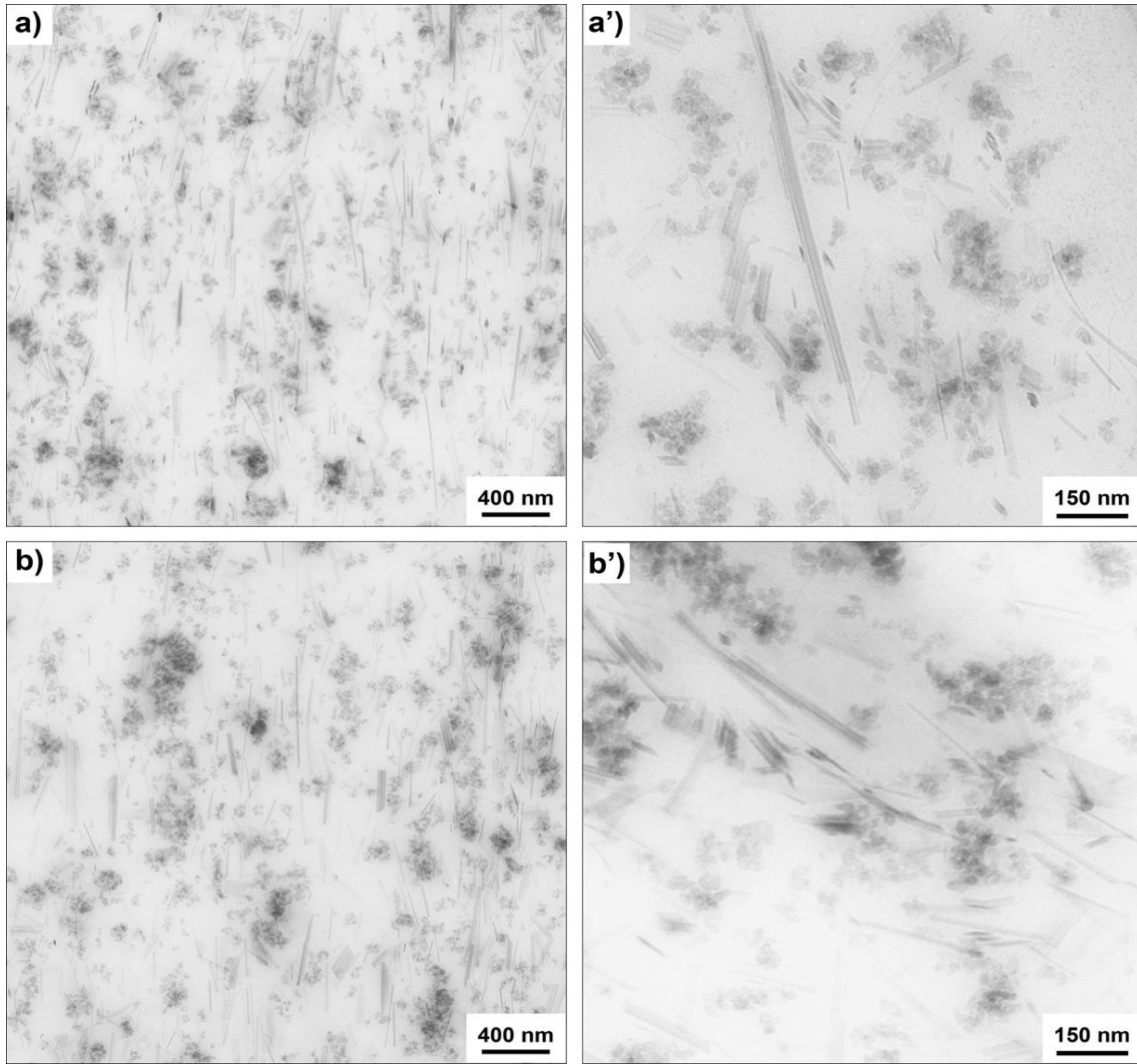
372 The TanDelta values of NCs prepared by MB result higher than those prepared with traditional melt
373 blending compounding. This could be related to poorer interdiffusion of the two filler networks, and
374 in a lower effect of the presence of nanoclays, resulting in a lower suppression of the silica self-
375 interacting forces (filler-filler interactions). This is also justified by the lower shear forces
376 developed during the mixing when using a MB approach.

377 Thus, the use of hybrid filler systems, especially those based on mSep and SiO₂, appears promising,
378 since they produce a remarkable reduction of Payne effect and rolling resistance, without
379 originating negative effects on the reinforcement. This peculiar behaviour envisages a favourable
380 compatibility between mSep and SiO₂ fillers and, in turn, the formation of an effective collaborative
381 network at the nanoscale level.

382 To support this hypothesis, double filled NCs were investigated by TEM analysis and
383 morphological observations were correlated to the dynamic-mechanical data. TEM images of
384 Sep+SiO₂/NR, MB-Sep+SiO₂/NR, mSep+SiO₂/NR and MB-mSep+SiO₂/NR samples are reported
385 in Fig. 2 and 3. The analysis carried out at different magnifications reveals a rather complex spatial
386 distribution of both silica nanoparticles and sepiolite fibers, which relies on both the NC preparation
387 method and the sepiolite kind.

388 In the Sep+SiO₂/NR sample (Fig. 2a,a'), the distribution of both fillers appears fairly homogeneous.
389 At low magnification (images not shown), large agglomerations with elongated shapes, generally
390 oriented in one direction and constituted by only Sep fibers or silica particles are detectable; among
391 them, silica aggregates, sub-micrometric Sep bundles, and isolated fibers are also found at higher
392 magnification (Fig. 2a'). The observed morphology does not highlight any specific interaction
393 between spherical SiO₂ particles and Sep fibers, and supports the similarity of G' and TanDelta
394 values of this sample to those of SiO₂/NR.

395



396

397 **Fig. 2** TEM images at different magnifications of (a, a') Sep+SiO₂/NR and (b, b') MB-
 398 Sep+SiO₂/NR samples.

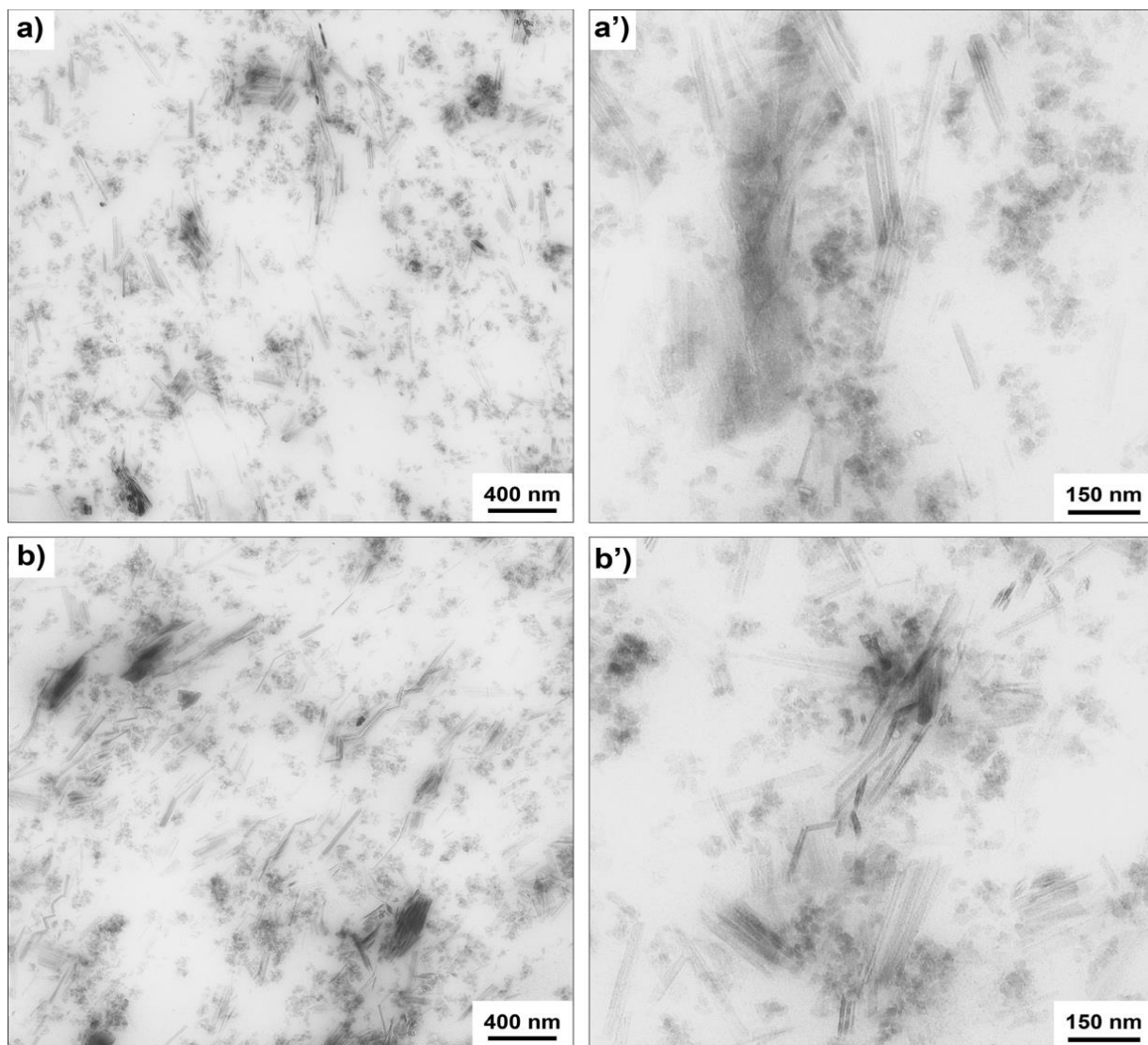
399

400 The preparation method involving the pre-dispersion of Sep in the MB (MB-Sep+SiO₂/NR sample)
 401 results in composites where a slightly less homogenous and finer distribution of the organoclays is
 402 detectable (Fig. 2b). Large filler agglomerations are not observed at low magnification (images not
 403 shown), but only sub-micrometric silica aggregates and Sep bundles, together with numerous
 404 isolated Sep needles. The hybrid filler networking does not appear continuous and homogeneous for
 405 the presence of self-assembled Sep domains with occluded rubber and partially oriented fibers (Di

406 Credico et al., 2018); moreover, any particular affinity between the two fillers is observed at higher
407 magnifications (Fig. 2b').

408 TEM images of NCs prepared with mSep and SiO₂ hybrid filler (Fig. 3) show a significantly
409 different morphology compared to of composites containing untreated Sep (Fig. 2). In
410 mSep+SiO₂/NR sample, obtained by traditional melt blending, both mSep bundles and silica
411 aggregates of elongated shapes (2 - 5 μm length) and preferentially aligned in one direction are
412 found at low magnification (images not shown). The presence of a larger number of micrometric
413 bundles (as those shown in Fig. 3a) suggests interactions between the fibers higher than those
414 observed for Sep, probably due to the high number of surface silanol sites and the reduced particles
415 size (Di Credico et al., 2018) of these treated fibers. A high number of isolated Sep needles and
416 superstructures of sub- or micrometric dimensions, composed by sepiolite fibers and silica
417 nanoparticles connected by thin polymer films, are noticeable at higher magnification (Fig. 3a').
418 These morphological features seem to support the existence of a cooperative hybrid filler network.

419 The morphology observed in the MB-mSep+SiO₂/NR sample (Fig. 3b,b'), which is characterized
420 by a fine mSep dispersion with a relevant number of isolated Sep needles and sub-micrometric
421 superstructures (Fig. 3b') similar to those observed in the mSep+SiO₂/NR sample (Fig. 3a'), further
422 endorse these considerations/hypothesis. Also, in this case, the mSep particles in the superstructures
423 appeared preferentially aligned in one direction and the affinity between fibers and silica aggregates
424 is in line with the reduced Payne effect and hysteresis previously discussed.



425

426 **Fig. 3** TEM images at different magnifications of (a, a') mSep+SiO₂/NR and (b, b') MB-
 427 mSep+SiO₂/NR samples.

428 Moreover, both filler distribution and dispersion result improved with respect to those of the sample
 429 obtained with the traditional procedure, as already observed for the hybrid NCs containing Sep.

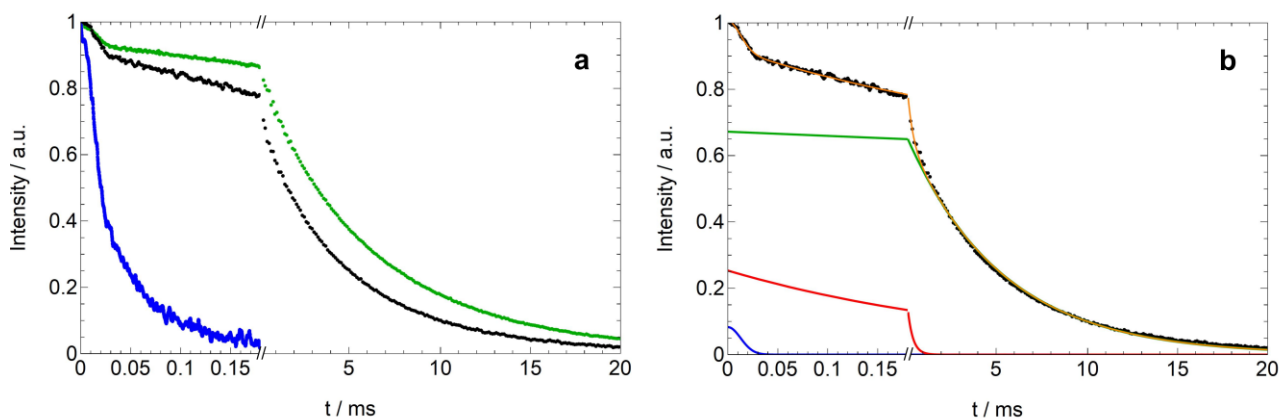
430 In summary, the morphological survey suggest the formation, within the rubber matrix, of
 431 cooperative superstructures due to the self-assembly of sepiolite and silica nanoparticles containing
 432 occluded rubber, when the secondary filler is mSep, which is obtained by a controlled acid
 433 treatment and is characterized by shorter fibers and higher surface silanol bonding sites (Di Credico
 434 et al., 2018). These peculiar characteristics of mSep bring about significant interactions between

435 mSep and silica, which result in a promoted self-assembly of the two fillers in a collaborative
436 hybrid network, improving dynamic-mechanical performances and, in particular, significantly
437 reducing the Payne effect.

438 The influence of the simultaneous presence of two different filler systems and of the preparation
439 techniques on the dynamic properties of the NCs at a molecular level, was studied by low-
440 resolution solid state NMR techniques, which exploit the measurement of ^1H T_2 relaxation times to
441 distinguish and quantify protons belonging to environments with different molecular mobility.

442 In particular, on resonance FID and CPMG decays were acquired for double filled NCs and for all
443 the pure components present in the formulations, by combining MSE and CPMG experiments
444 (three examples are shown in Fig. 4a). The MSE pulse sequence was exploited to refocus the short
445 decaying signal deriving from protons in rigid environments. On the other hand, the CPMG
446 sequence was used to measure ^1H T_2 associated with the slow-decaying components of the ^1H
447 signals, which in a free decay can be shortened by non-dynamics contributions, such as the
448 magnetic susceptibility of the sample and/or fluctuations of the external magnetic field.

449 For all the double filled NCs, the combined MSE/CPMG relaxation curves are well reproduced by
450 fitting a linear combination of three different functions (the case of MB-mSep+SiO₂/NR is shown in
451 Fig. 4b), each characterized by a T_2 (T_2^i) and a weight percentage ($W^i\%$). Specifically, one
452 Gaussian function (gau) and two exponential functions (exp1, exp2) were used to reproduce the
453 decays associated to protons in rigid ($T_2 = 10\text{-}50\ \mu\text{s}$), intermediate ($T_2 = 50\text{-}1000\ \mu\text{s}$) or mobile (T_2
454 $> 1\ \text{ms}$) environments, respectively. The fitting of MSE/CPMG relaxation curves allows to quantify
455 the three domains with different mobility and to determine all the T_2 values (Table 4). At a first
456 inspection, we can observe a similar behavior of all double filled NCs with a predominant domain
457 of mobile protons (66-67%) with T_2 of about 5 and 6 ms for vulcanized and crude samples,
458 respectively; a 23-25% of protons display an intermediate mobility and only 8-11% of protons
459 result in a rigid environment.



460

461 **Fig. 4** (a) ^1H MSE FID of mSep (blue) and combined MSE/CPMG relaxation curves of NR (green)
 462 and vulcanized MB-mSep+SiO₂/NR (black). (b) Experimental (black) and best-fit (orange line)
 463 MSE/CPMG relaxation curve of vulcanized MB-mSep+SiO₂/NR. Together with the total fitting
 464 function (orange line) and the single contributions of the Gaussian (blue line), intermediate-T₂ (red
 465 line), and long-T₂ (green line) exponential functions are shown.

466 To get quantitative information on the molecular mobility of NR in connection with the fillers
 467 network, we performed an analysis by comparing the weights obtained from the fitting of the
 468 experimental curves and the theoretical weights, which were calculated under the assumption that
 469 all the components maintain the degree of mobility of their pure state also in the NCs.

470 Practically, the theoretical evaluation was done in several steps, which include the experimental
 471 determination of the hydrogen content for all the pure components by construction of a calibration
 472 curve with standard solid compounds (technical details on the calculations are reported in SI; a
 473 similar procedure for the estimation of the proton content in the pristine materials was already
 474 reported (D'Arienzo et al., 2018). By exploiting the MSE experiment, the percentage of hydrogen
 475 deriving from each pure compound on the total hydrogen content in the NCs was calculated; then,
 476 based on MSE FID's or combined MSE/CPMG relaxation curves, the weights of protons in rigid,
 477 intermediate and mobile fraction were determined for each pure compound. By combining these
 478 results, the theoretical weights of protons in rigid, intermediate and mobile fraction for the NCs

479 were evaluated (Table 4). To notice, since Sep+SiO₂/NR and MB-Sep+SiO₂/NR (and
480 mSep+SiO₂/NR and MB-mSep+SiO₂/NR) contain the same amounts of pure compounds, their
481 theoretical evaluation results identical. The calculation of the theoretical weights does not take into
482 account possible changes of molecular mobility induced by the physical interactions between the
483 materials present in the composite, such as rubber-filler interactions, which may also differ
484 depending on the type of procedure used to prepare the composites.

485 Therefore, in order to unveil such plausible changes, the theoretical results obtained for
486 Sep+SiO₂/NR and on mSep+SiO₂/NR samples (equal to those for the corresponding samples
487 prepared by LCT) have been compared with the T₂ analysis of the MSE/CPMG relaxation curves
488 obtained for NC samples prepared through the formation of MBs or by traditional melt blending
489 (Table 4). From the comparison of the theoretical estimates and the analyses of the real composites,
490 several differences can be observed, the most relevant being that real samples, containing both
491 spherical and anisotropic fillers, show larger weights of the domain with intermediate mobility,
492 associated with smaller percentage of protons in very mobile domains. It is also worth noting that
493 such difference (about 5-8%), even if not very big, is reproducible in all hybrid filler NCs and might
494 be explained with the formation of a loosely-bound rubber, displaying a T₂ of about 200-250 μs.
495 Indeed, in the literature values of T₂ of the order of 10–20 μs have been associated to “tightly bound
496 rubber” (i.e., chains experiencing a very restricted overall mobility), as distinguished from “loosely
497 bound rubber”, experiencing a larger degree of mobility and associated to ¹H T₂ values of the order
498 of several tens/hundreds of μs (O’Brien et al., 1976; Ou et al., 1996; Borsacchi et al., 2018).

499 It is worth noting that, in the case of crude samples, the percentage of protons in rigid environments
500 remains almost the same compared to the theoretical evaluation; conversely, for the vulcanized
501 sample the weight of the rigid component is slightly lower. This might be caused by the presence of
502 crystalline compounds in the crude samples, which may react or melt during vulcanization.

503

504 **Table 4.** Results of the analysis of the MSE/CPMG ^1H FIDs* recorded for both crude and
 505 vulcanized composite samples, and theoretical weights obtained as described in the text.

	Gau	Exp1	Exp2
	W¹% (T₂¹/μs)	W²% (T₂²/μs)	W³% (T₂³/ms)
Sep+SiO₂/NR crude	11 (16)	23 (212)	66 (6.4)
MB-Sep+SiO₂/NR crude	10 (16)	24 (208)	66 (6.2)
mSep+SiO₂/NR crude	11 (17)	22 (266)	67 (6.2)
MB-mSep+SiO₂/NR crude	10 (17)	23 (254)	67 (6.2)
Sep+SiO₂/NR	8 (15)	25 (170)	67 (5.2)
MB-Sep+SiO₂/NR	8 (16)	25 (215)	67 (5.3)
mSep+SiO₂/NR	9 (16)	25 (258)	66 (5.2)
MB-mSep+SiO₂/NR	9 (17)	25 (280)	66 (5.2)
Theoretical for Sep+SiO₂/NR and MB-Sep+SiO₂/NR	11	17	71
Theoretical for mSep+SiO₂/NR and MB-mSep+SiO₂/NR	11	17	71

506 *The values of ^1H T₂ relaxation times obtained for each of the three functions (Gau, Exp1, Exp2)
 507 used to fit the MSE/CPMG relaxation curves are reported in brackets and expressed in μs (or ms in
 508 the case of Exp2).
 509

510 Importantly, the different procedures used to prepare the composites did not significantly affect the
 511 distribution of the domains with different mobility, evidencing the fact that the LCT has a similar
 512 effect on proton dynamics in the final product compared to melt blending.

513 Thus, NMR measurements indicate the formation of a noticeable fraction of loosely bound rubber
 514 in hybrid filled NCs, even if do not highlight significant differences among samples prepared with
 515 Sep or mSep. This can be related to the fact that ^1H T₂ are sensitive to very local nuclear
 516 environments and therefore only probe short range interactions (on sub-nanometric scale). In other
 517 words, it is plausible that short range interactions are very similar for Sep and mSep, while

518 rheological and mechanical behaviour can be more influenced by longer range morphologies (on a
519 hundred of nanometres scale), which result different for NCs containing treated and untreated Sep,
520 as evidenced by TEM images.

521

522 **4. Conclusions**

523 Rubber-based NCs containing silica and sepiolite were prepared by combining LCT and melt
524 blending processes, with the aim of evaluating the effect of the self-assembly of hybrid fillers
525 (silica/sepiolite) and of the combined preparation technique on the final materials properties.

526 A critical evaluation of rheological and mechanical properties of final hybrid filled NC highlights
527 that: i) the combined procedure is a simple and effective method to obtain high-performance rubber
528 NCs; ii) the use of double white fillers, having different aspect ratios, allows to obtain a good trade-
529 off between efficient reinforcement and low Payne effect, in particular when the secondary filler is
530 mSep. Morphological TEM analysis suggests that this result may be associated with the formation
531 of cooperative fillers network based on the synergic interaction of both sepiolite and silica
532 nanoparticles with the polymer matrix, providing a higher polymer–filler interactions. In agreement
533 with this hypothesis, ^1H Time Domain NMR experiments indicate the formation of a noticeable
534 fraction of loosely bound rubber in hybrid filled NCs.

535 This study, even if referred to Sep/SiO₂ double fillers, provides clear evidence of the significant role
536 of self-assembly of hybrid nanofillers to produce a collaborative filler network and thus advanced
537 rubber materials.

538

539 **Appendix A. Supplementary data**

540 Supplementary data include: loss modulus vs strain of NCs materials (Fig. S1); methods for the
541 theoretical determination of ^1H mobility in NCs by Time Domain NMR; fitting of MSE and
542 MSE/CPMG experiments for NR, SiO₂, Sep and mSep (Fig. S2); total hydrogen content for all pure

543 compounds (Table S1); contribution of each component to the hydrogen content of NCs (Table S2);
544 and results of FID's analysis recorded for all pure compounds (Table S3).

545

546 **Author contributions**

547 Irene Tagliaro: Investigation, Data curation, Writing – originadraft, Writing - review & editing.

548 Elkid Cobani: Investigation, Data curation. Elisa Carignani, Francesca Martini, Francesca Nardelli:

549 Investigation, Data curation, Writing - review & editing. Lucia Conzatti, Paola Stagnaro:

550 Investigation, Data curation, Formal analysis, Writing - review & editing. Massimiliano

551 D'Arienzo, Luca Giannini, Roberto Scotti, Luciano Tadiello: Data curation, Formal analysis,

552 Writing - review & editing. Barbara Di Credico: Conceptualization, Supervision; Validation;

553 Visualization, Data curation, Formal analysis, Writing - original draft, Writing - review & editing.

554

555 **Declaration of Competing Interest**

556 The authors declare that they have no known competing financial interests or personal relationships

557 that could have appeared to influence the work reported in this paper.

558

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